



# Computational Analysis of the External Aerodynamics of the Unpowered X-57 Mod-III Aircraft

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# Acknowledgement

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# Outline

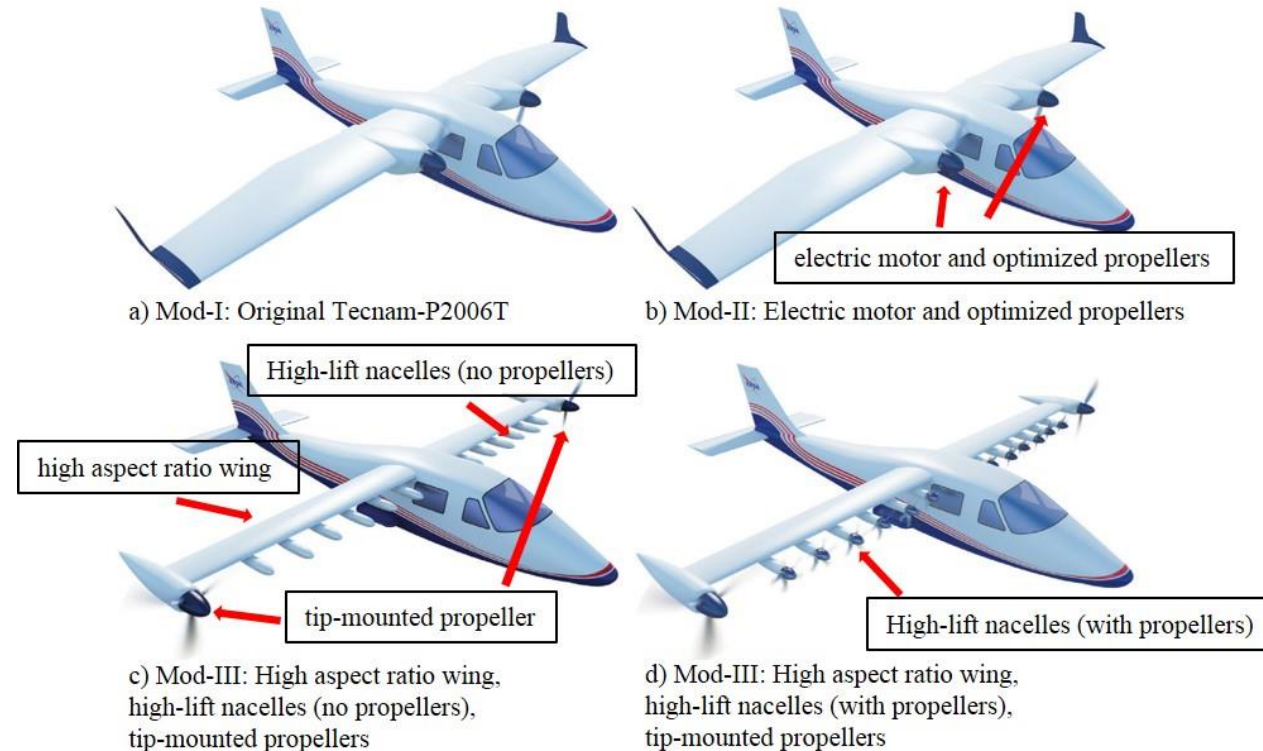
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- Introduction
- Method
- Results
- Conclusion
- Questions



# Introduction

- X-57 Program
  - Separated into multiple phases, denoted as “MOD”, to demonstrate various technologies
    - Electrical power-plant
    - Optimized high aspect ratio wing and high lift nacelle
    - Tip cruise motor for reducing induced drag
- Study focused on unpowered MOD-III
  - flow physics
  - differences in flow solution between CFD solvers
- Purpose of the study
  - Aerodynamic database generation for pilot-in-the-loop simulation
  - Understanding of the aerodynamics of the vehicle for flight safety
  - Baseline performance for powered simulation





# Method

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- STAR-CCM+ (v13.04.10)

- Used extensively at NASA AFRC for airworthiness analysis
- Grid
  - Unstructured polyhedral mesh
  - Half-span with symmetry boundary condition for symmetric flow, full-span for asymmetric flow simulation
- Solver
  - Steady state RANS
  - 2<sup>nd</sup> order Roe flux differencing scheme with algebraic multigrid solver with Gauss-Siedel relaxation scheme
  - Fully turbulent assumption, Spalart-Allmaras with rotational correction

- Launch Ascent Vehicle Analysis Framework

- Versatile NASA ARC developed framework consisting of multiple solvers
- Grid
  - Overset, structured, curvilinear grids
  - Full-span for all simulations
- Solver
  - Steady state RANS structured curvilinear solver
  - Second-order convective flux with Koren limiter
  - Fully turbulent flow assumption, Spalart-Allmaras turbulence rotational correction and quadratic constitutive relationship



# Result

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- Grid Refinement Study
- Angle of attack sweep
- Sideslip angle sweep



# Result – Grid Refinement Study

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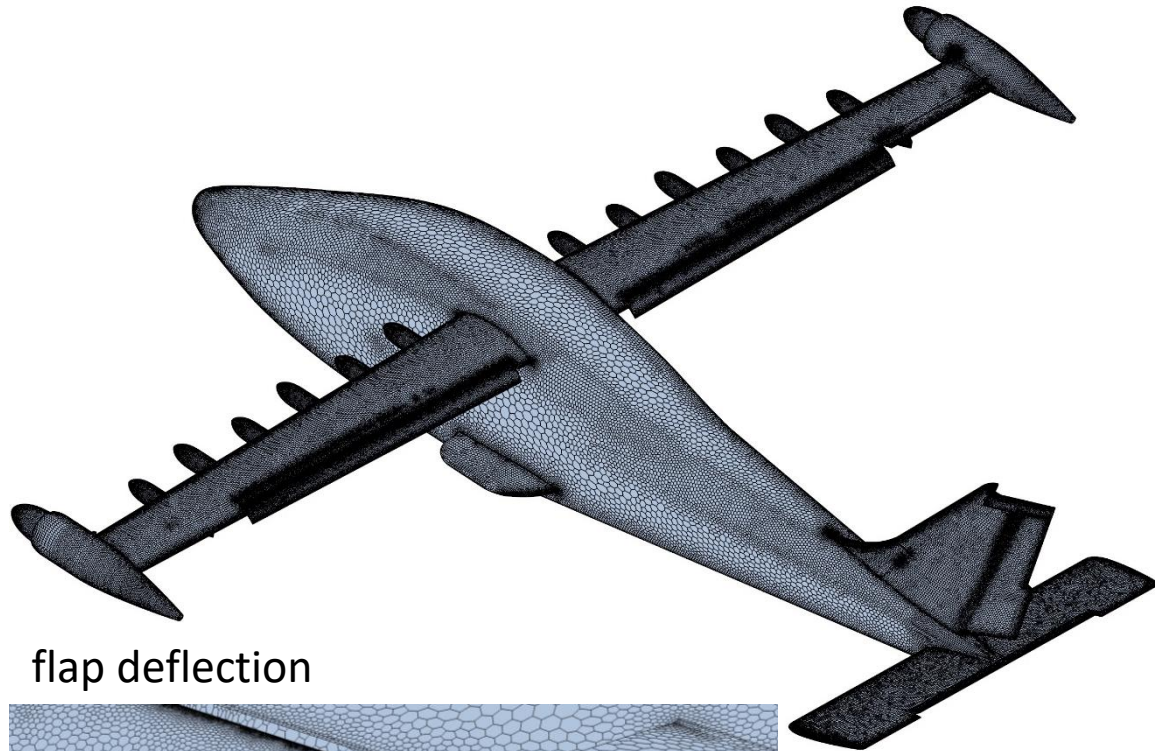
- Atmospheric Condition
  - Altitude 2500 ft, Mach 0.139, freestream velocity = 153.87 ft/s
  - density  $2.2078\text{E-}3\text{kg/m}^3$ , static pressure = 1931.9 lbf/ft<sup>2</sup>, static temperature 283.2K
  - Reynolds number  $9.21\text{E}5$
  - Angle of attack =  $10^\circ$ , Sideslip angle =  $20^\circ$
- Aircraft configuration
  - Aileron =  $-25^\circ$
  - Flap =  $30^\circ$
  - Rudder =  $-28^\circ$
  - Stabilator =  $-15^\circ$
  - Pitch trim tab =  $-18^\circ$



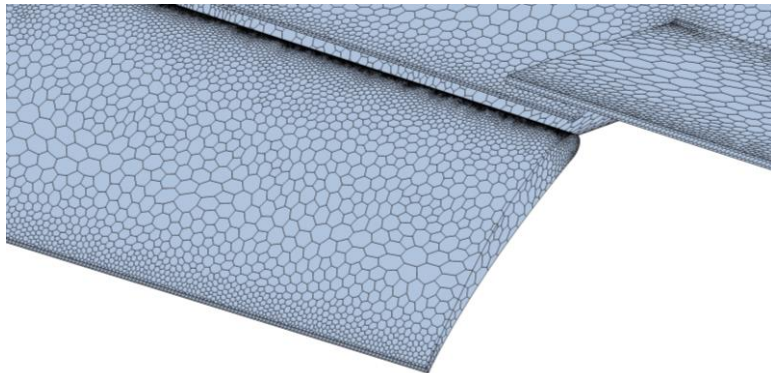


# Result – Grid Refinement Study

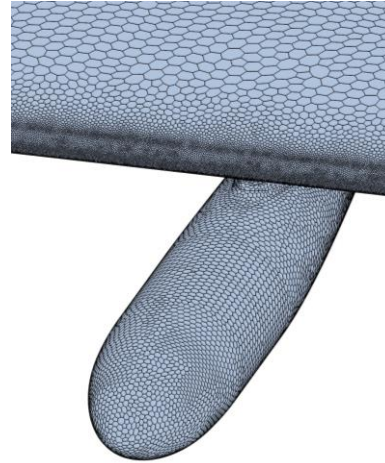
- STAR-CCM+ Polyhedral Grid (coarse grid shown for clarity)



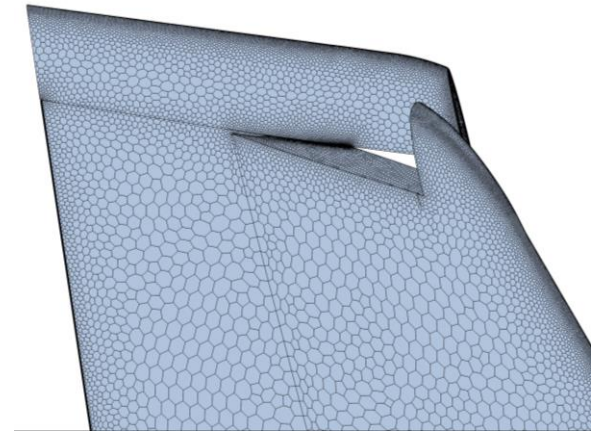
flap deflection



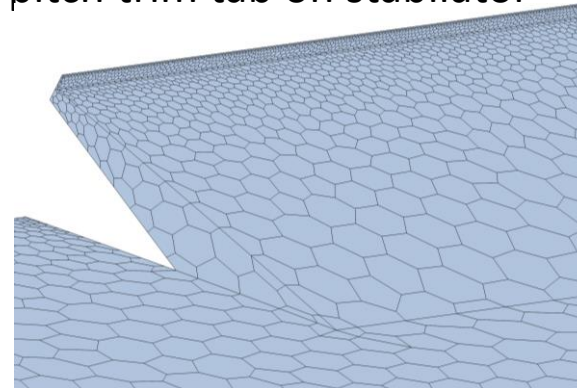
high lift nacelle



rudder deflection



pitch trim tab on stabilator



stabilator

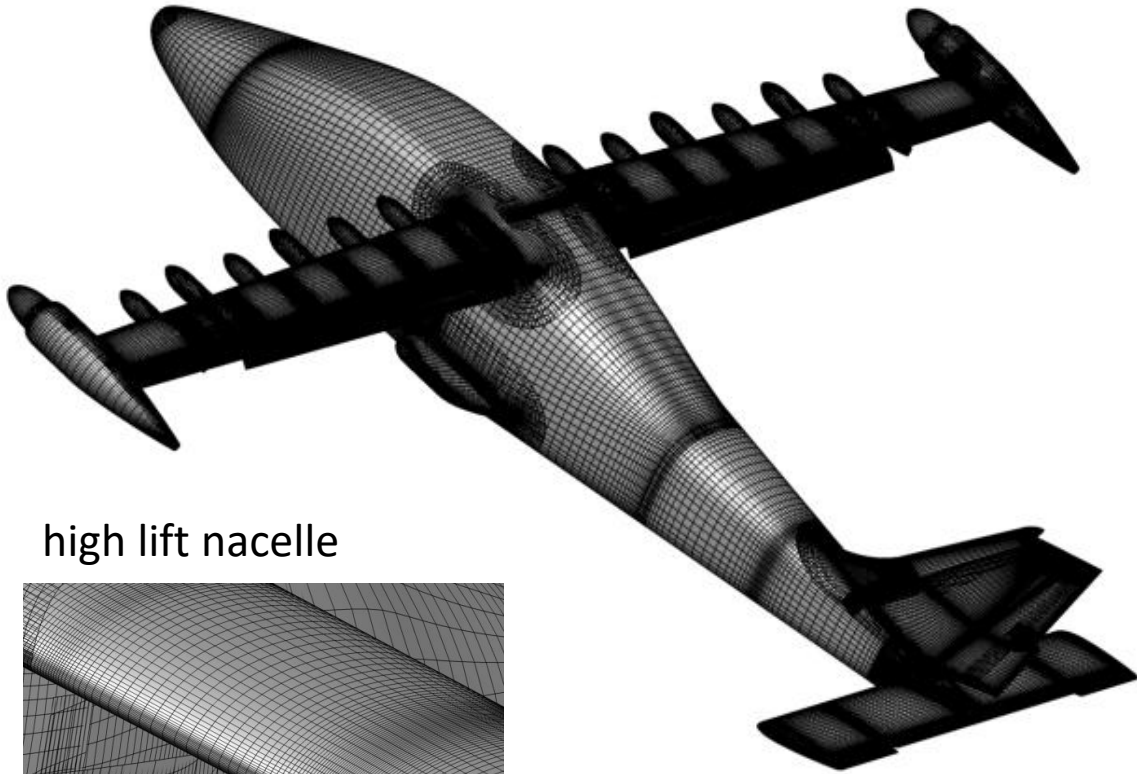




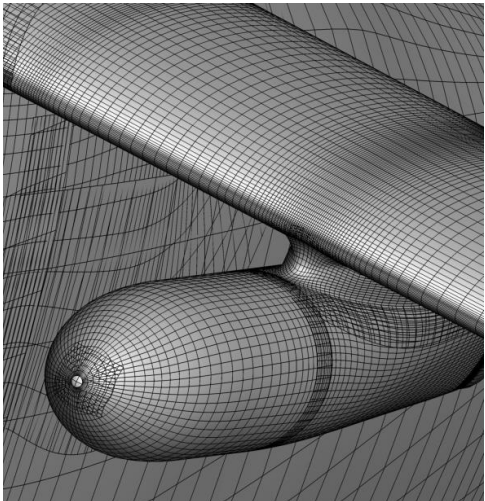


# Result – Grid Refinement Study

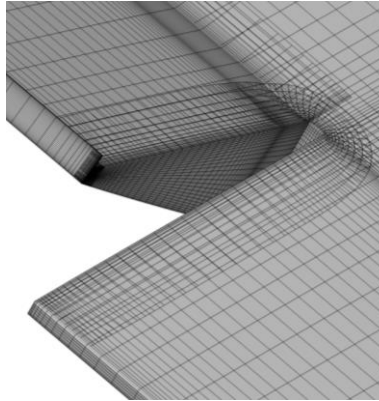
- LAVA structured overset curvilinear grid (coarse grid shown for clarity)



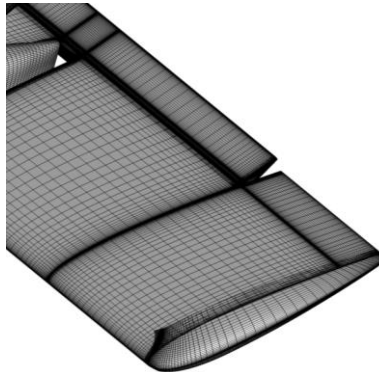
high lift nacelle



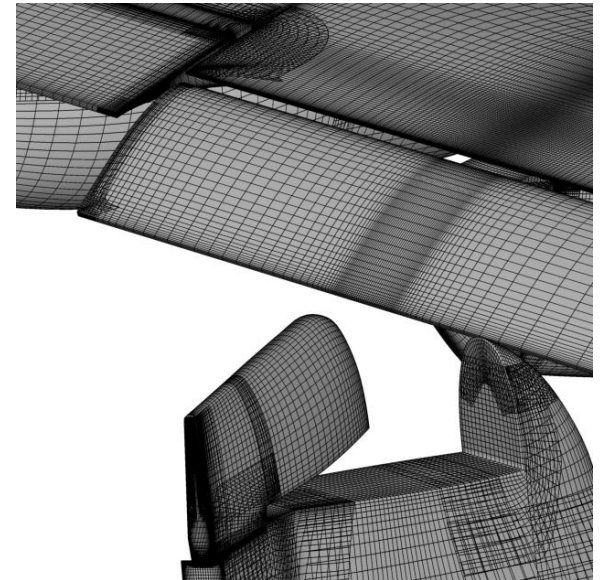
pitch trim tab on stabilator



stabilator



flap and rudder deflection





# Result – Grid Refinement Study

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- STAR-CCM+
  - 3 resolutions: 45e6 Cells (coarse), 77e6 Cells (medium), 126e6 Cells (fine)
- LAVA
  - 5 resolutions: 60.1e6 nodes (coarse), 95.2e6 nodes (medium), 248.6e6 nodes (fine), 312.6e6 nodes (very-fine), 425.7e6 nodes (extra-fine)



# Result – Grid Refinement Study

| STAR-CCM+ grid resolution | $C_D$   | $C_L$   | $C_Y$    | $C_I$   | $C_m$   | $C_n$   |
|---------------------------|---------|---------|----------|---------|---------|---------|
| coarse (45e6 cells)       | 0.30394 | 1.46749 | -0.61327 | 0.01631 | 2.41895 | 0.12050 |
| medium (77e6 cells)       | 0.30623 | 1.47778 | -0.61585 | 0.02004 | 2.41327 | 0.12257 |
| fine (126e6 cells)        | 0.30797 | 1.47193 | -0.61886 | 0.01982 | 2.38941 | 0.12337 |

| STAR-CCM+ grid resolution | $C_D$ error, % | $C_L$ error, % | $C_Y$ error, % | $C_I$ error, % | $C_m$ error, % | $C_n$ error, % |
|---------------------------|----------------|----------------|----------------|----------------|----------------|----------------|
| coarse (45 mil. cell)     | -1.1           | -0.3           | -0.9           | -17.7          | 1.2            | -2.3           |
| medium (77 mil. cell)     | -0.5           | 0.4            | -0.5           | 1.1            | 1.0            | -0.6           |

Although relative error  $C_I$  is large, the values are small and coarse mesh chosen to accommodate the large number of runs for limited computing resource



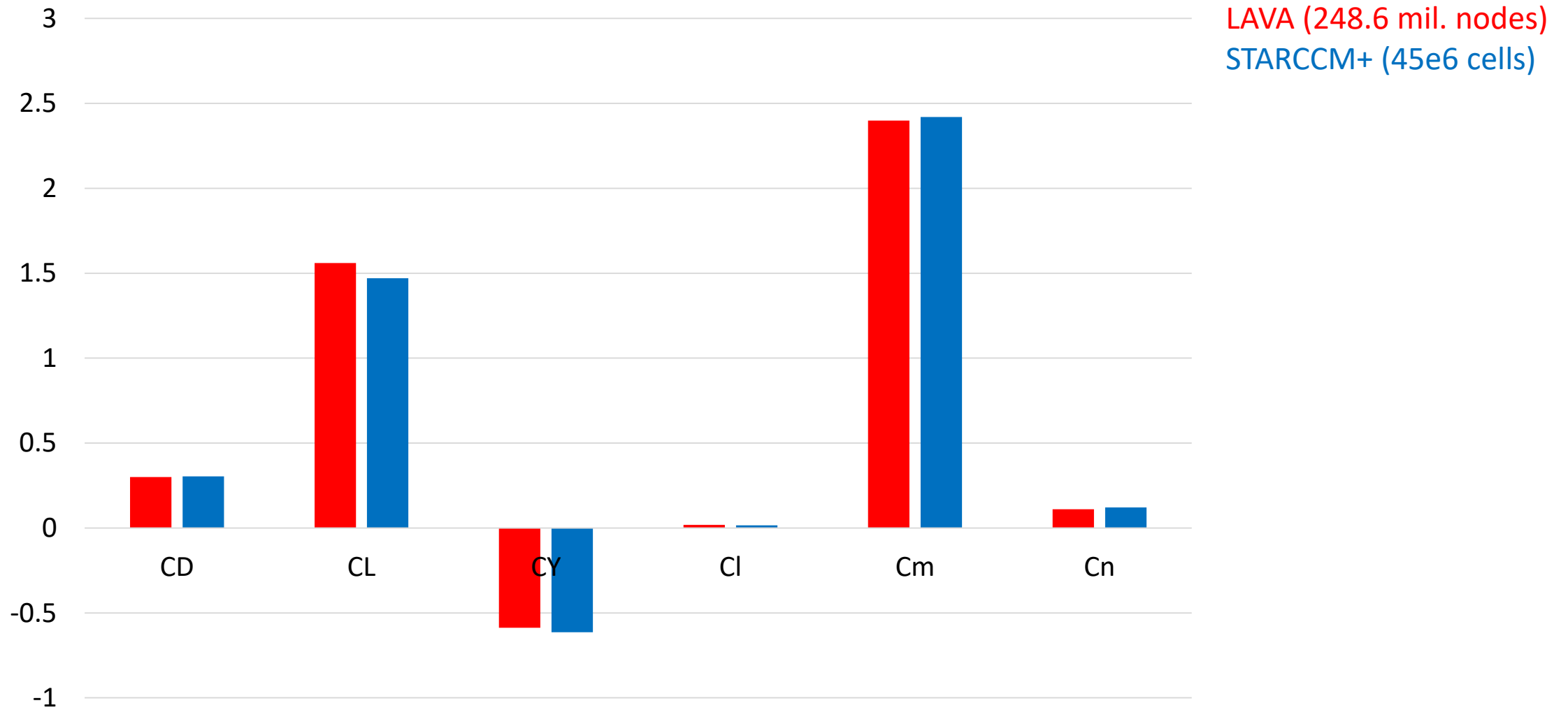
# Result – Grid Refinement Study

| LAVA grid resolution           | $C_D$          | $C_L$       | $C_Y$          | $C_I$         | $C_m$        | $C_n$         |
|--------------------------------|----------------|-------------|----------------|---------------|--------------|---------------|
| coarse (60.1 mil. nodes)       | 0.3024         | 1.57        | -0.6053        | 0.0135        | 2.396        | 0.1119        |
| medium (95.2 mil. nodes)       | 0.29838        | 1.55        | -0.595         | 0.016         | 2.404        | 0.1117        |
| <b>fine (248.6 mil. nodes)</b> | <b>0.30036</b> | <b>1.56</b> | <b>-0.5876</b> | <b>0.0181</b> | <b>2.398</b> | <b>0.1106</b> |
| very-fine (312.6 mil. nodes)   | 0.30265        | 1.56        | -0.5844        | 0.0226        | 2.402        | 0.1121        |
| extra-fine (425.7 mil nodes)   | 0.30237        | 1.56        | -0.582         | 0.0239        | 2.401        | 0.1126        |

| LAVA grid resolution           | $C_D$ error, % | $C_L$ error, % | $C_Y$ error, % | $C_I$ error, % | $C_m$ error, % | $C_n$ error, % |
|--------------------------------|----------------|----------------|----------------|----------------|----------------|----------------|
| coarse (60.1 mil. nodes)       | -0.01          | -0.64          | -4.00          | 43.51          | 0.21           | 0.62           |
| medium (95.2 mil. nodes)       | 1.32           | 0.51           | -2.23          | 33.05          | -0.12          | 0.80           |
| <b>fine (248.6 mil. nodes)</b> | <b>0.66</b>    | <b>-0.26</b>   | <b>-0.96</b>   | <b>24.27</b>   | <b>0.12</b>    | <b>1.78</b>    |
| very-fine (312.6 mil. nodes)   | -0.09          | -0.32          | -0.41          | 5.44           | -0.04          | 0.44           |



# Result – Grid Refinement Study





# Result

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- Grid Refinement Study
- Angle of attack sweep
- Sideslip angle sweep



# Result – Angle of attack sweep

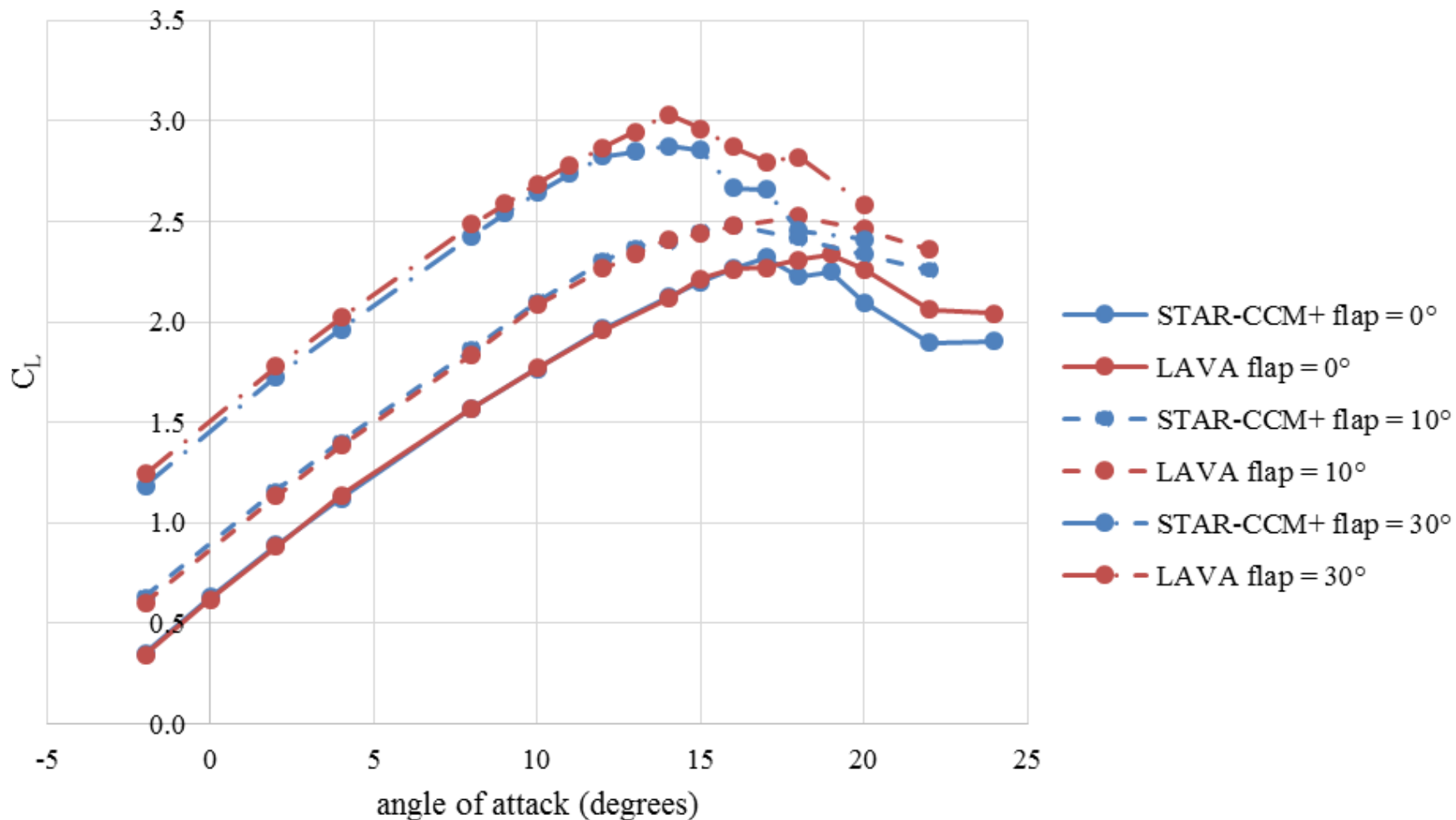
- 3 flap settings –  $0^\circ$  (cruise) ,  $10^\circ$  (take-off),  $30^\circ$  (landing)
- Control surfaces in neutral position (no deflection)

|                                      | Flap = $0^\circ$ | Flap = $10^\circ$ | Flap = $30^\circ$ |
|--------------------------------------|------------------|-------------------|-------------------|
| Altitude, ft                         | 8000             | 2500              | 2500              |
| Mach                                 | 0.233            | 0.149             | 0.139             |
| Density, slug/ft <sup>3</sup>        | 1.8628E-3        | 2.20782E-3        | 2.20782E-3        |
| Static pressure, lbf/ft <sup>2</sup> | 1571.9           | 1931.9            | 1931.9            |
| Static temperature, K                | 272.3            | 283.2             | 283.2             |
| Coefficient of viscosity, slug/ft/s  | 3.57532E-7       | 3.68708E-7        | 3.68708E-7        |
| Reynolds number                      | 1.32E6           | 9.875E5           | 9.21E5            |





# Result – Angle of attack sweep

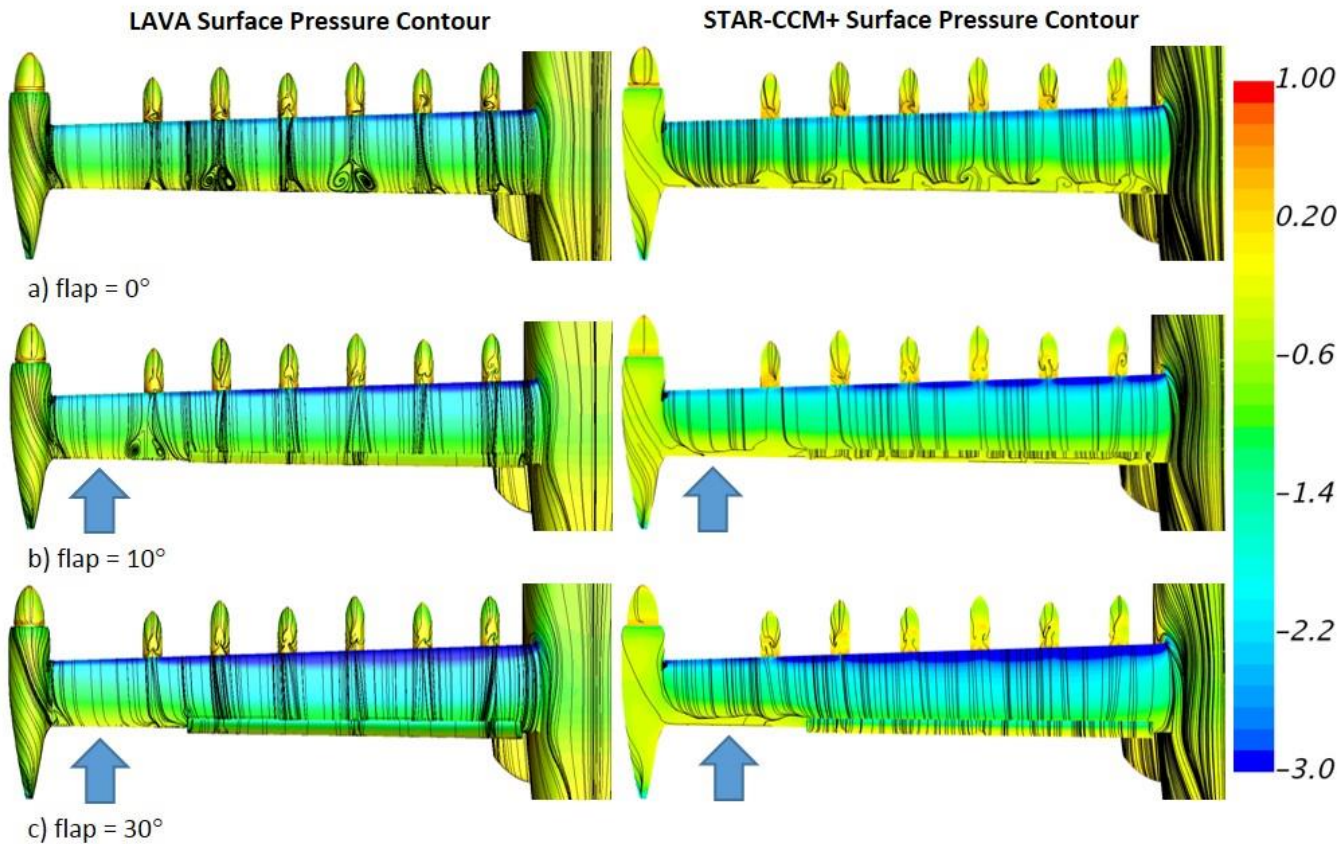


- Lift dependency on flap deflection
  - lift increases with increase in flap deflection angle
  - Angle of attack for maximum lift decreases with increase in flap deflection
- Differences in solver
  - lift at high angle of attack
  - Increase in discrepancy with increase in flap deflection angle at linear region



# Result – Angle of attack sweep

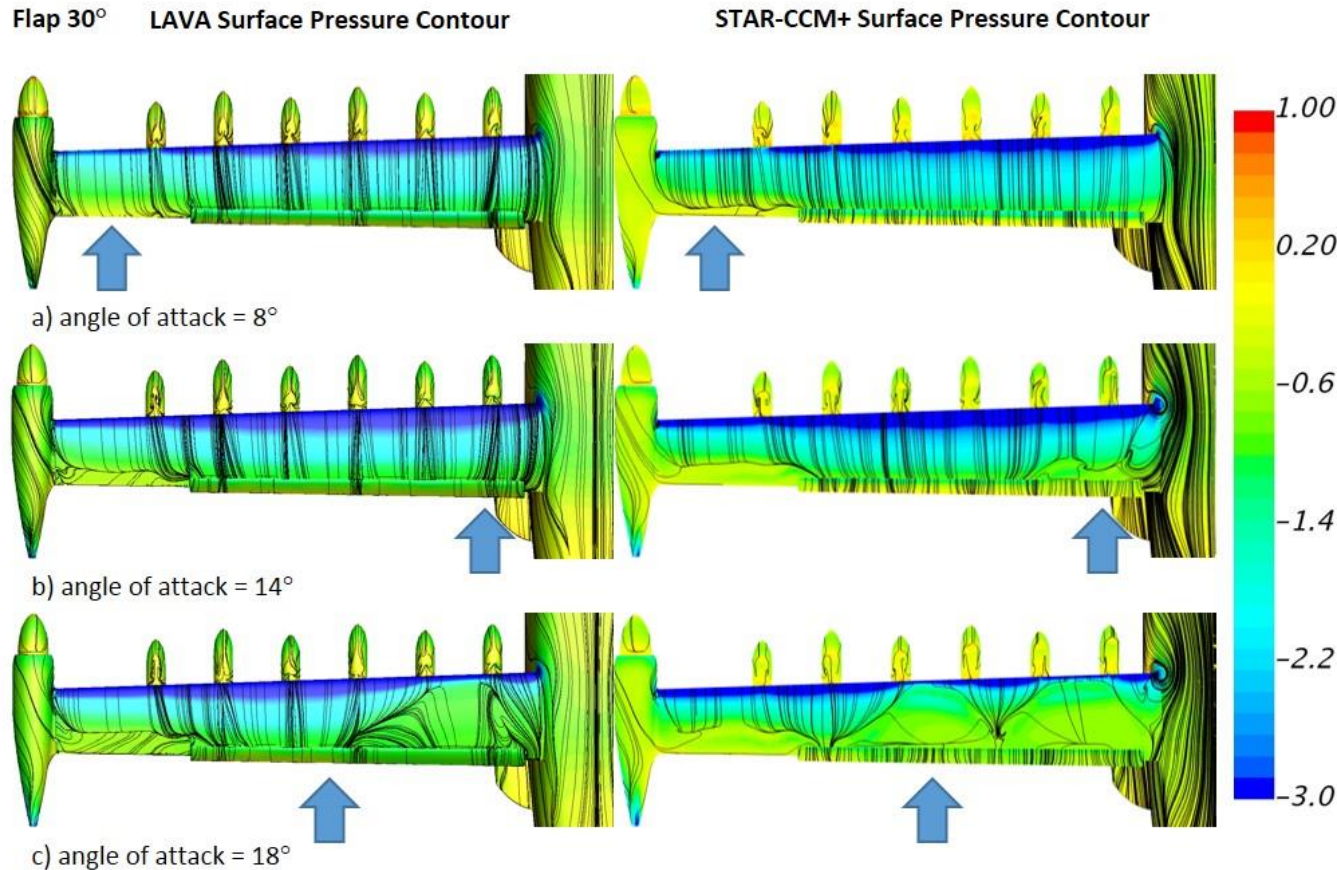
Angle of attack =  $8^\circ$



- Increase in solution discrepancy in lift with increase in flap deflection angle at linear region
- STAR-CCM+ solution show flow separation at outboard wing that is not show in LAVA for  $10^\circ$  and  $30^\circ$  flap deflection



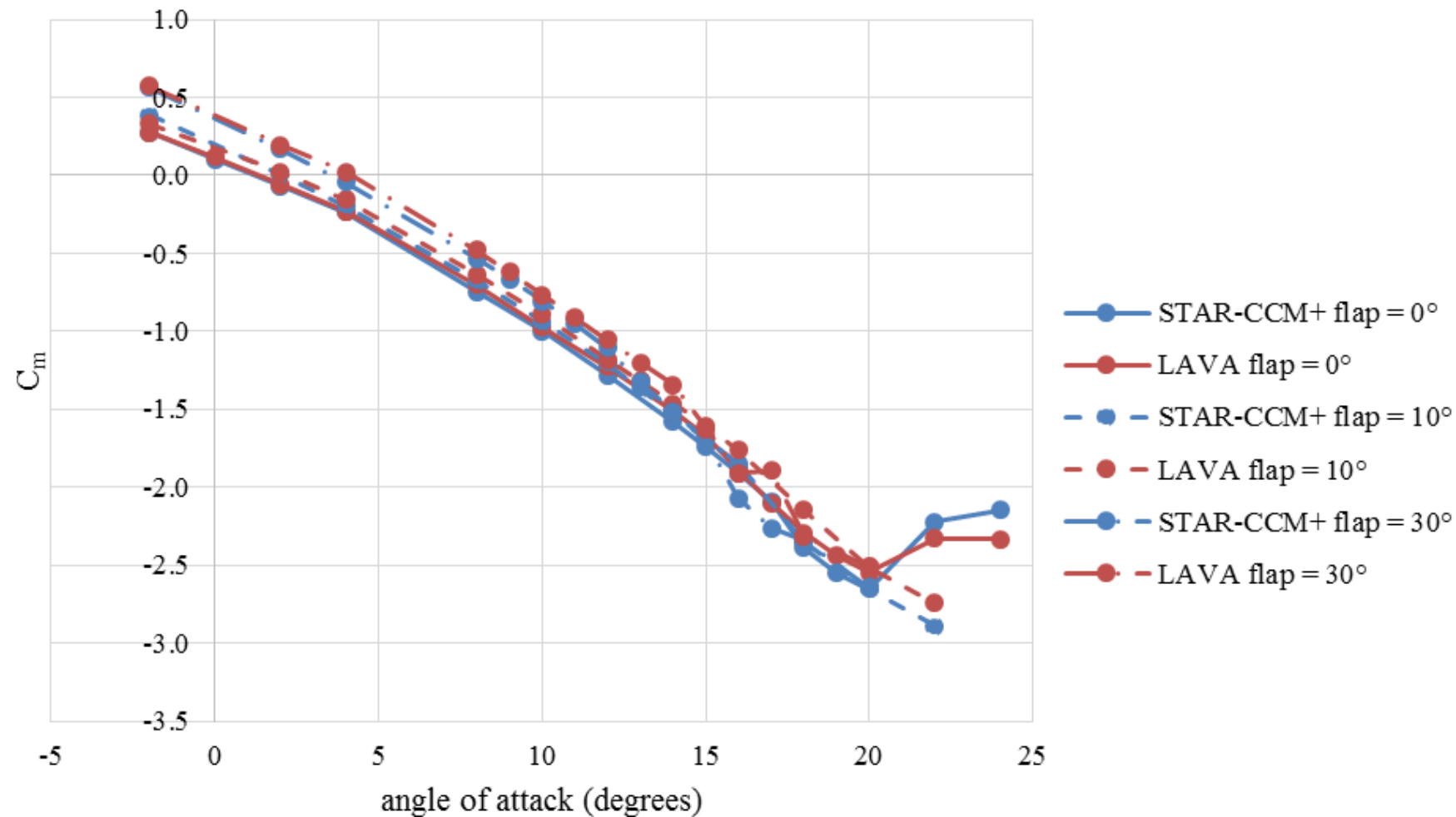
# Result – Angle of attack sweep



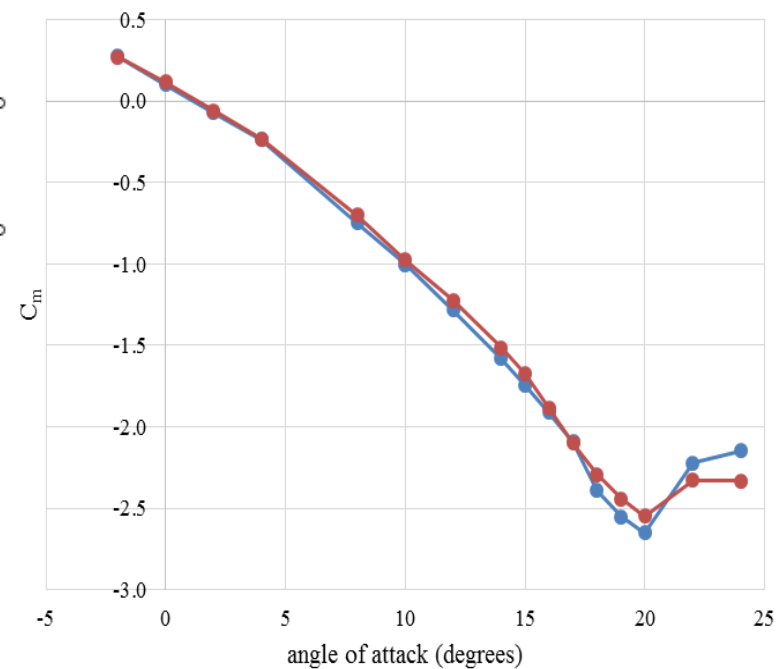
- Increase in solution discrepancy in lift at high angle of attack
- STAR-CCM+ solution show larger region of separated flow at higher angle of attack compared to LAVA



# Result – Angle of attack sweep



- Higher pitching moment with higher flap deflection angle
- Sharp increase in pitching moment for 0° flap angle at 20° angle of attack

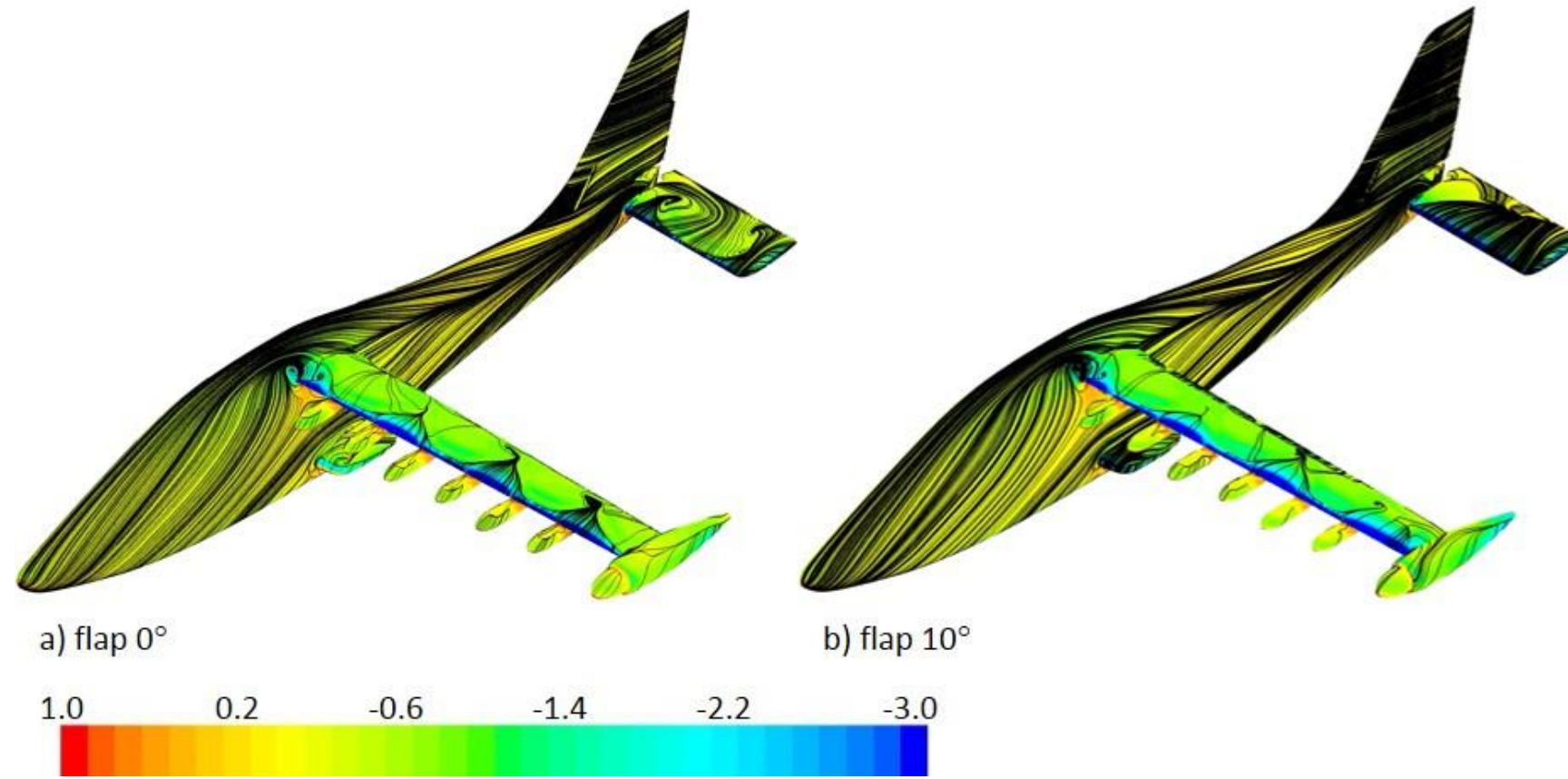






# Result – Angle of attack sweep

Angle of attack =  $22^\circ$ , surface pressure contour



- Large flow separation shown on the upper surface of stabilator for  $0^\circ$  flap deflection configuration
- Flow separation shown on the upper surface of stabilator on  $10^\circ$  flap deflection configuration located to inboard and trailing edge



# Result

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- Grid Refinement Study
- Angle of attack sweep
- Sideslip angle sweep



# Result – Sideslip angle sweep

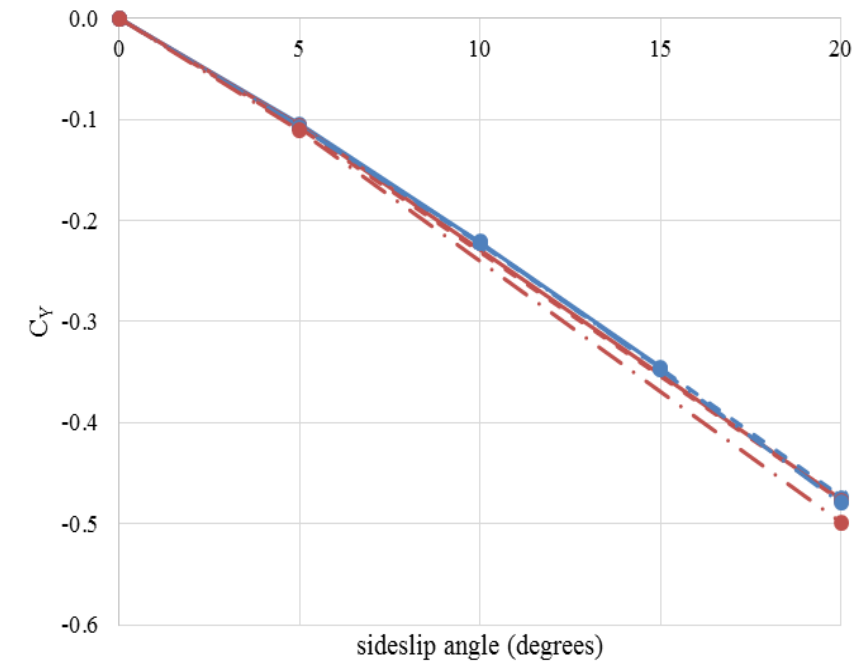
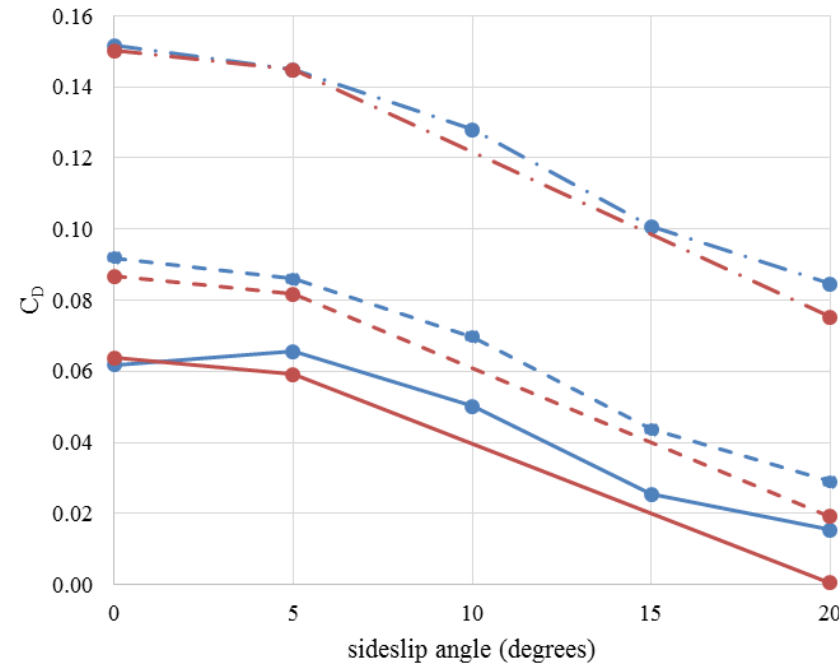
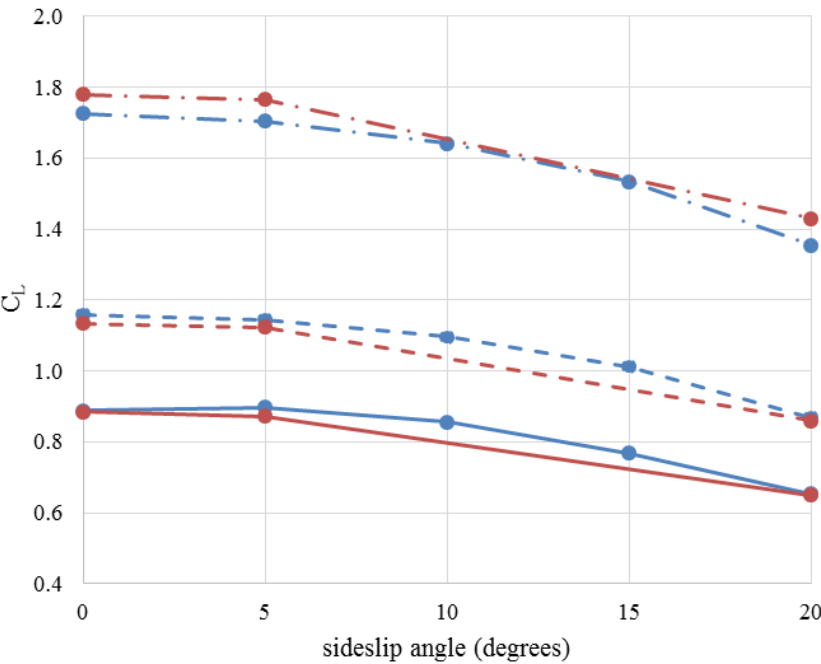
- 3 flap settings –  $0^\circ$  (cruise) ,  $10^\circ$  (take-off),  $30^\circ$  (landing)
- Control surfaces in neutral position (no deflection)

|  | <b>Flap = <math>0^\circ</math></b> | <b>Flap = <math>10^\circ</math></b> | <b>Flap = <math>30^\circ</math></b> |
|--|------------------------------------|-------------------------------------|-------------------------------------|
| <b>Altitude, ft</b>                        | 8000                               | 2500                                | 2500                                |
| <b>Mach</b>                                | 0.233                              | 0.149                               | 0.139                               |
| <b>Density, slug/ft<sup>3</sup></b>        | 1.8628E-3                          | 2.20782E-3                          | 2.20782E-3                          |
| <b>Static pressure, lbf/ft<sup>2</sup></b> | 1571.9                             | 1931.9                              | 1931.9                              |
| <b>Static temperature, K</b>               | 272.3                              | 283.2                               | 283.2                               |
| <b>Coefficient of viscosity, slug/ft/s</b> | 3.57532E-7                         | 3.68708E-7                          | 3.68708E-7                          |
| <b>Reynolds number</b>                     | 1.32E6                             | 9.875E5                             | 9.21E5                              |

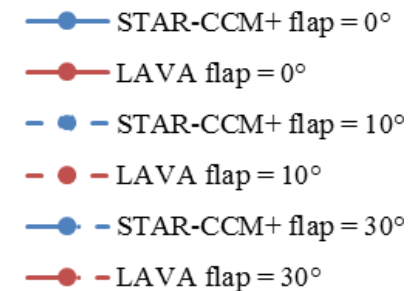




# Result – Sideslip angle sweep

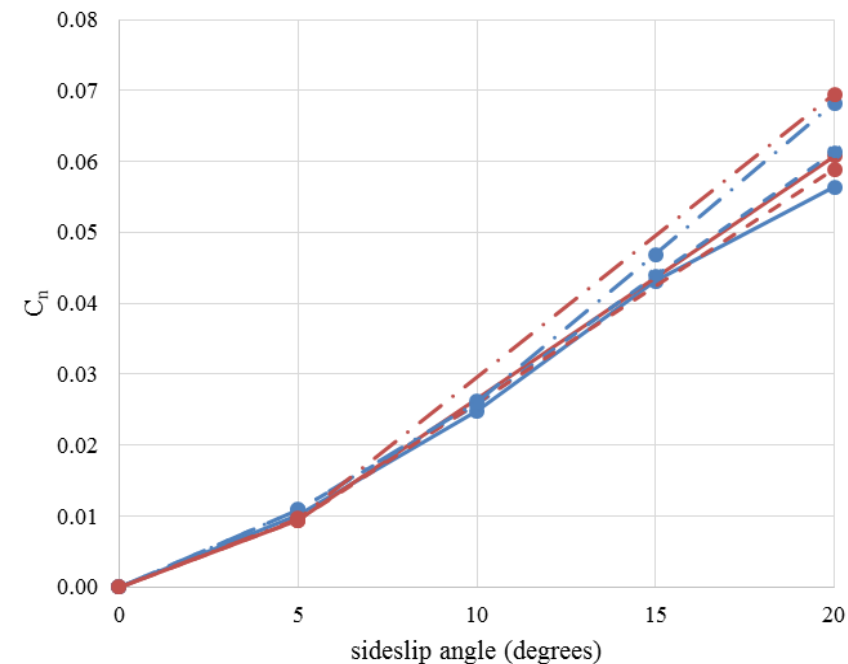
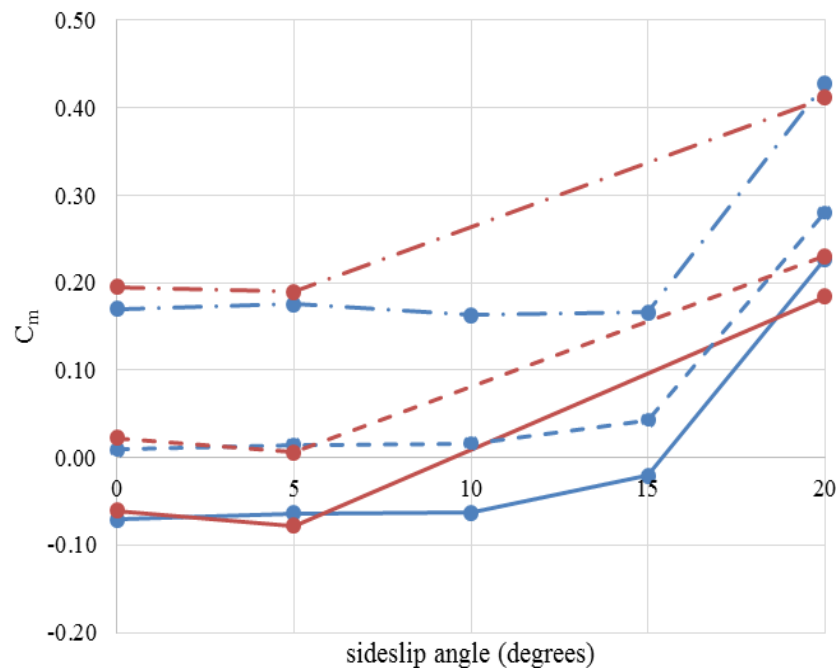
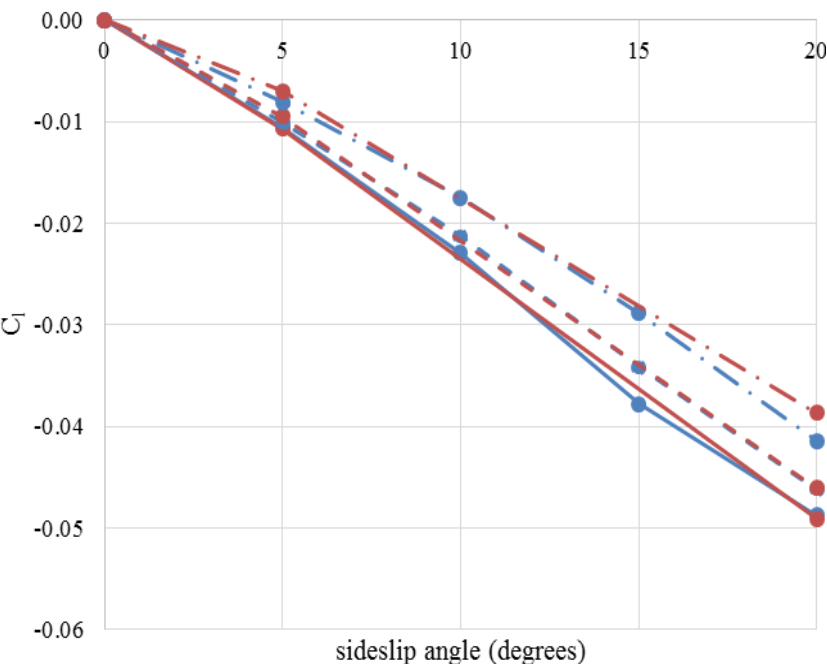


- Lift, drag, side forces all decrease with increasing sideslip angle
- Drag decreasing because it is in stability axis (increases when computed in wind axis)

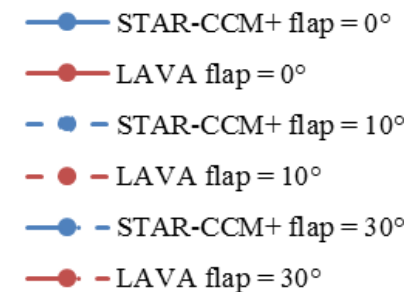




# Result – Sideslip angle sweep



- Rolling moment - 30° flap produces least amount of rolling moment
- Pitching moment - sharp increase in at 15° for all flap deflections
- Yawing moment - 30° flap produces least amount of rolling moment





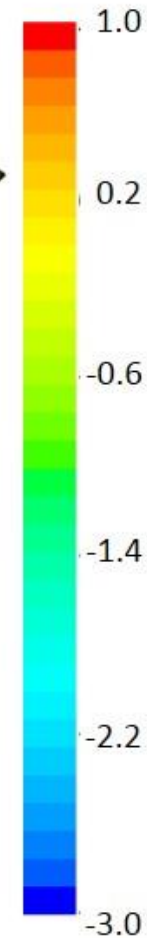
# Result – Sideslip angle sweep

surface pressure coefficient, Angle of attack =  $22^\circ$

a) flap =  $0^\circ$

b) flap =  $10^\circ$

c) flap =  $30^\circ$



- Increasing separation at leading edge of right wing root with increasing flap deflection
- Separated region at the leading edge of rudder



# Conclusion

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- Unpowered X-57 MOD-III configuration analyzed
- Angle of attack sweep and sideslip angle sweep presented
- STAR-CCM+ and LAVA solution comparison
  - flow visualization show that solution compare well at low angle of attack
  - Difference in predicted separation behavior at higher angle of attack



QUESTION?